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# Hydrogen production by steam reforming of methanol in a micro-channel reactor coated with Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst

Short communication

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### Abstract

Hydrogen production by steam reforming of methanol is studied over Cu/Zn-based catalysts (Cu/ZnO, Cu/ZnO/Al<sub>2</sub>O<sub>3</sub>, Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub>). Cu/Zn-based catalysts are derived from hydrotalcite-like precursors prepared by a co-precipitation method. The catalysts are characterized by N<sub>2</sub>O chemisorption, XRD, and BET surface area measurements. ZrO<sub>2</sub> added to the Cu/Zn-based catalyst enhances copper dispersion on the catalyst surface. Among the catalysts tested, Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> exhibits the highest methanol conversion and the lowest CO concentration in the outlet gas. A micro-channel reactor coated with a Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst in the presence of an undercoated Al<sub>2</sub>O<sub>3</sub> buffer layer exhibits higher methanol conversion and lower CO concentration in the outlet gas than in the absence of an undercoated Al<sub>2</sub>O<sub>3</sub> buffer layer. The micro-channel reactor with a undercoated Al<sub>2</sub>O<sub>3</sub> buffer layer produces large amounts of hydrogen compared with one without a buffer layer. The undercoated Al<sub>2</sub>O<sub>3</sub> buffer layer enhances the adhesion between catalysts and micro-channel walls, which leads to improvement in reactor performance.

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## 1. Introduction

Methanol is readily available as a hydrogen source and can be converted into hydrogen-rich gas at moderate temperatures. If methanol is produced from renewable sources, its reforming does not cause a net increase of carbon dioxide in the atmosphere [1]. Thus, steam reforming of methanol has been extensively studied to produce hydrogen for proton-exchange membrane fuel cells (PEMFCs) [2–6]. A typical catalyst systems employed in the steam reforming of methanol include Cu-based catalyst impregnated on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> [7], Cu-based monolith [8], Cu/ZnO catalyst promoted by ZrO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> [9], Zr-containing CuO/ZnO catalyst [10], and Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst [11]. It is known that steam reforming of methanol yields a product gas containing up to 75% hydrogen [12]. Equilibrium

0378-7753/\$ - see front matter © 2005 Elsevier B.V. All rights reserved. doi:10.1016/j.jpowsour.2005.11.095 conversion in the steam reforming of methanol reaches around 100% at 150 °C and atmospheric pressure [13]. Therefore, steam reforming of methanol has been recognized as a promising route to produce hydrogen for PEMFCs. Nevertheless, the process must meet several requirements, among which one of the most important is that the product gas stream should contain extremely low level of carbon monoxide (a catalyst poison). For the efficient production of hydrogen from methanol, an autothermal micro-channel reactor has been designed and its performance reported [14].

In this work, hydrogen production by stream reforming of methanol is examined over a series of Cu/Zn-based catalysts (Cu/ZnO, Cu/ZnO/Al<sub>2</sub>O<sub>3</sub>, Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub>) in a continuous flow fixed-bed reactor. After the catalyst screen test, microchannel reactors coated with Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst in the presence/absence of a Al<sub>2</sub>O<sub>3</sub> buffer layer are designed, and the effect of undercoated Al<sub>2</sub>O<sub>3</sub> buffer layer on reactor performance is evaluated.

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## 2. Experimental

A series of Cu/Zn-based catalysts (Cu/ZnO, Cu/ZnO/Al<sub>2</sub>O<sub>3</sub>, Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub>) were derived from hydrotalcite-like precursors prepared by co-precipitation of metal nitrates in an aqueous solution. Metal nitrates with the desired mole ratios were dissolved in distilled water. The total metal concentration in the aqueous solution was 1 M. A 0.3 M Na<sub>2</sub>CO<sub>3</sub> aqueous solution was then added with vigorous stirring under a stream of nitrogen at 60 °C (pH  $\approx$  9). The precipitates were aged for 3 h and then recovered by filtration, followed by washing with distilled water. The solid product was dried at 100 °C for 12 h, and then calcined at 350 °C for 12 h with an air stream to yield the final form. Prior to the catalytic reaction, each catalyst was reduced in a mixed stream of H<sub>2</sub> (10%) and N<sub>2</sub> (90%) at 350 °C for 3 h.

The catalysts were characterized by X-ray diffraction (Rigaku, D/MAX-2000) and BET surface area analysis (Micromeritics, ASAP 2010). The specific surface area of  $Cu^0$  in each catalyst was measured by N<sub>2</sub>O chemisorption by means of the method described elsewhere [15]. Temperature programmed reduction (TPR) measurements were performed to investigate copper dispersion and reducibility.

A micro-channel reactor, which had a micro-channel sheet with four holes for the flow path and 34 parallel channels of rectangular shape, was used in this work. The dimensions of the micro-channels were 300  $\mu$ m in width, 200  $\mu$ m in depth, and 20 mm in length. Two types of micro-channel sheets coated with Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst were designed, namely, (i) the micro-channel walls were directly coated with Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst, (ii) Al<sub>2</sub>O<sub>3</sub> was introduced as a buffer layer between the Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst and the micro-channel wall to improve the adhesion between the two components. Coating of the Al<sub>2</sub>O<sub>3</sub> buffer was undertaken by the atomic layer deposition (ALD) method. The thickness of the undercoated Al<sub>2</sub>O<sub>3</sub> buffer layer was about 0.1  $\mu$ m.

## 3. Results and discussion

The physicochemical properties of the prepared catalysts are summarized in Table 1. The Cu/ZnO catalyst showed the lowest BET surface-area (47.5 m<sup>2</sup> g<sup>-1</sup>). On addition of the Al<sub>2</sub>O<sub>3</sub> and ZrO<sub>2</sub> structural promoters, the surface area increases up to 90.8 m<sup>2</sup> g<sup>-1</sup> for Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> and 129.7 m<sup>2</sup> g<sup>-1</sup> for Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub>. The Cu<sup>0</sup> surface area determined from N<sub>2</sub>O chemisorption monotonically increases on addition of Al<sub>2</sub>O<sub>3</sub> and ZrO<sub>2</sub>. The Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst exhibites the highest Cu<sup>0</sup> surface area. This indicates that the addition of

Table 1 Physicochemical properties of catalysts



Fig. 1. XRD patterns of (a) Cu/ZnO, (b) Cu/ZnO/Al\_2O\_3, and (c) Cu/ZnO/ZrO\_2/Al\_2O\_3.

structural promoters such as  $ZrO_2$  and  $Al_2O_3$  provides a large catalyst surface on which copper can be dispersed. Combination of the two metal oxides rather than an individual metal oxide is more efficient. This result is consistent with the findings of Velu et al. [16,17], who demonstrated that substitution of aluminum with zirconium improved copper dispersion and also reducibility.

The XRD patterns of the calcined catalysts are shown in Fig. 1. Peaks indicative of aluminum, zinc, and zirconium phases are not detected, which implies that aluminum, zinc, and zirconium phases are in an amorphous-like or a micro-crystallite state. Only CuO phases appear in a crystal form. The peak intensities of CuO in the Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst are much weaker than those in the Cu/ZnO and Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalysts. This indicates that ZrO<sub>2</sub> improves copper dispersion in the Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst with a highly dispersed Cu species may show an excellent catalytic performance in the reaction.

The TPR profiles of the freshly calcined and reoxidized catalysts are shown in Fig. 2. The profile for the Cu/ZnO catalyst shows at least three overlapping peaks. The first reduction starts at 135 °C, and H<sub>2</sub> consumption is maximum at 190 °C. There is also a shoulder peak at about 200 °C, and reduction is completed at around 250 °C. Reoxidation and subsequent reduction of Cu/ZnO increases the particle size, as indicated by the fact that the temperature required for complete reduction increased up to about 290 °C. The freshly calcined Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst is completely reduced at a higher temperature than the Cu/ZnO catalyst. The main peak appears at 240 °C with a long

Catalyst	Composition (mole%)				BET surface area $(m^2 g^{-1})$	$Cu^0$ area $(m^2 g^{-1})$
	Cu	Zn	Zr	Al		
Cu/ZnO	50	50	_	_	47.5	20.8
Cu/ZnO/Al <sub>2</sub> O <sub>3</sub>	50	25	_	25	90.8	23.7
Cu/ZnO/ZrO <sub>2</sub> /Al <sub>2</sub> O <sub>3</sub>	50	25	18.75	6.25	129.7	25.9



Fig. 2. TPR profiles of freshly calcined (thin line) and reoxidized (thick line) catalysts.

tail extending to 350 °C, which suggests the existence of large CuO crystallites or a strong interaction between copper and support. A strong interaction between copper and the support can also be confirmed from the fact that the XRD peak intensities associated with CuO are relatively weak in the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst. After reoxidation, the TPR peak of the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub>

catalyst unexpectedly shifts towards a lower temperature. This indicates that the interaction between copper and support in the Cu/ZnO/Al<sub>2</sub>O<sub>3</sub> catalyst decreases after reoxidation. On the other hand, the Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst exhibits the lowest reduction temperature (190 °C) before and after reoxidation, which indicates the formation of small CuO particles. This, in turn, leads to a high dispersion of Cu species on the catalyst surface. This result is consistent with the Cu<sup>0</sup> surface area in Table 1, where the highest dispersion of Cu species is observed in the Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst. Both the reduction profiles of Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst obtained before and after reoxidation are narrow and almost symmetrical, which suggest a narrow particle size distribution and a homogeneous material composition.

Catalyst screen tests were carried out in a fixed-bed quartz reactor to find the optimum reaction conditions by measuring methanol conversion and CO level in the product gas. The reaction experiments were conducted at temperature of a 180-270 °C with a H<sub>2</sub>O:CH<sub>3</sub>OH feed mole ratio of 0.6–1.5 for 50 mg of catalyst sample. The total feed flow rate diluted with a helium carrier was 50 ml/min. From a series of catalytic reactions performed with variation of reaction temperature and H<sub>2</sub>O:CH<sub>3</sub>OH mole ratio, a reaction temperature of 260 °C and a H<sub>2</sub>O:CH<sub>3</sub>OH mole ratio of 1:3 are found to be the optimum reaction conditions (although the catalytic reaction data are not shown here). The



Fig. 3. Methanol conversion and CO level in product gas from steam reforming of methanol at 260 °C and a H<sub>2</sub>O:CH<sub>3</sub>OH mole ratio of 1:3.



Fig. 4. Performance of micro-channel reactor coated with Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst for steam reforming of methanol at 260 °C and a H<sub>2</sub>O:CH<sub>3</sub>OH mole ratio of 1:3 (open symbol, without buffer layer; closed symbol, with buffer layer).

typical catalytic performance obtained at these optimum reaction conditions is given in Fig. 3. The Cu/ZnO/ZrO<sub>2</sub> catalyst shows a slightly enhanced catalytic performance compared with the Cu/ZnO catalyst. On the other hand, the Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst exhibits the highest methanol conversion and the lowest CO concentration in the outlet gas. The catalyst containing ZrO<sub>2</sub> is highly efficient in the steam reforming of methanol. This may be due to high dispersion of small sized Cu species caused by the addition of a ZrO<sub>2</sub> promoter.

The effect of an undercoated  $Al_2O_3$  buffer layer on the performance of the micro-channel reactor coated with  $Cu/ZnO/ZrO_2/Al_2O_3$  catalyst in the steam reforming of methanol performed at 260 °C and H<sub>2</sub>O:CH<sub>3</sub>OH mole ratio of 1:3 is shown in Fig. 4. The micro-channel reactor with an undercoated  $Al_2O_3$  buffer layer shows a higher methanol conversion and a lower CO concentration in the outlet gas. The methanol conversion is over 90% and the CO concentration in the outlet gas is less than 0.1%. Furthermore, the micro-channel reactor with an undercoated  $Al_2O_3$  buffer layer produces large amounts of hydrogen compared with the one without buffer layer. It is believed that the undercoated  $Al_2O_3$  buffer layer enhances the adhesion between catalysts and micro-channel walls, and thus, it improves the reactor performance.

### 4. Conclusions

Hydrogen production by steam reforming of methanol was examined over a series of Cu/Zn-based catalysts. N<sub>2</sub>O chemisorption, TPR, and XRD results show that ZrO<sub>2</sub> added to Cu/Zn-based catalysts plays an important role in enhancing copper dispersion and in forming small sized copper particles on the catalyst surface. Among the catalysts tested, the Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst exhibits the highest methanol con-

version and the lowest CO concentration in the outlet gas. A micro-channel reactor coated with Cu/ZnO/ZrO<sub>2</sub>/Al<sub>2</sub>O<sub>3</sub> catalyst in the presence of undercoated Al<sub>2</sub>O<sub>3</sub> buffer layer gives higher methanol conversion and lower CO concentration in the outlet gas than that in the absence of an undercoated buffer layer. The former produces larger amounts of hydrogen. It is concluded that the undercoated Al<sub>2</sub>O<sub>3</sub> buffer layer enhances the adhesion between catalysts and micro-channel walls, and thus improves reactor performance.

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